

## APPENDIX A

% BEGINNING OF PSEUDO CODE

5       % compute scale factor A, and time constants a, b from physical system  
      % parameters

$A = V_{max} * K_t / (R_e * R_m + K_t * K_b) * l * k;$

10    p1 =  $1/J_m/I_e * (-I_e * R_m - R_e * J_m + \sqrt{I_e^2 * R_m^2 - 2 * R_e * R_m * I_e * J_m}$   
       $+ R_e^2 * J_m^2 - 4 * K_t * K_b * I_e * J_m}) / 2;$   
      p2 =  $1/J_m/I_e * (-I_e * R_m - R_e * J_m - \sqrt{I_e^2 * R_m^2 - 2 * R_e * R_m * I_e * J_m}$   
       $+ R_e^2 * J_m^2 - 4 * K_t * K_b * I_e * J_m}) / 2;$

15       a = max(-p1,-p2)  
      b = min(-p1,-p2)

% make initial guesses for step durations

20       et1 = 1;  
      et2 = .005;  
      et3 = 1;

% set maximum iteration count

25       Nmax = 1000;

      for j = 1:Nmax

          % save old values of step time intervals

30       et3old = et3;

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et2old = et2;
et1old = et1;

% iterate for switch times using fixed voltage level Vmax

5
et3 = -log(1.0 / 2.0 - exp(-et1 * a) / 2 + exp(-et2 * a)) / a;
et2 = 1/b * log(2.0) + 3 * et3 - 1/b * log(2 * exp(1/A * b * X) * exp(et3
    * b) - sqrt(4.0) * sqrt(exp(1/A * b * X)) * exp(et3 * b) *
    sqrt(exp(1/A * b * X)+exp(et3 * b)^2 - 2 * exp(et3 * b)));
10
et1 = - (-2 * A * et2 + 2 * A * et3 - X) / A;

if norm([et3old - et3 et2old - et2 et1old - et1], inf) <= eps * 2
    break
end
15
if j==Nmax
    error(['error - failure to converge after ', num2str(Nmax),'
        iterations'])
end
end

20
% round up pulse duration to nearest sample interval,
% convert to intervals between steps to make sure that voltage
% requirements will not increase (beyond Vmax).

25
dt1=ceil((et1 - et2) / dt) * dt;
dt2=ceil((et2 - et3) / dt) * dt;
dt3=ceil((et3) / dt) * dt;

et123 = [et1, et2, et3]

30
% convert back to total step duration.

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et1 = dt1 + dt2 + dt3;
et2 = dt2 + dt3;
et3 = dt3;

5      % In the following, the original constraints equations involving XF1, XF2,
      % and XF3 have been modified to include a variable voltage level applied
      at
      % each step (instead of the fixed maximum (+/-) Vmax).

10     % The original equations for XF1, XF2, and XF3 follow:
      %       $XF_1(t_{end}) = V_0F_1(t_{end} - t_0) - 2V_0F_1(t_{end} - t_1) + 2V_0F_1(t_{end} - t_2)$ 
      %       $XF_2(t_{end}) = V_0F_2(t_{end} - t_0) - 2V_0F_2(t_{end} - t_1) + 2V_0F_1(t_{end} - t_2)$ 
      %       $XF_3(t_{end}) = V_0F_3(t_{end} - t_0) - 2V_0F_2(t_{end} - t_1) + 2V_0F_1(t_{end} - t_2)$ 

15     % And the modified equation including adjustable relative levels of
      voltage
      % L1, L2 and L3 are:
      %       $XF_1(t_{end}) = L_1V_0F_1(t_{end} - t_0) - L_2V_0F_1(t_{end} - t_1) + L_3V_0F_1(t_{end} - t_2)$ 
      %       $XF_2(t_{end}) = L_1V_0F_2(t_{end} - t_0) - L_2V_0F_2(t_{end} - t_1) + L_3V_0F_1(t_{end} - t_2)$ 
20     %       $XF_3(t_{end}) = L_1V_0F_3(t_{end} - t_0) - L_2V_0F_2(t_{end} - t_1) + L_3V_0F_1(t_{end} - t_2)$ 

      % And the corresponding constraint equations are:
      %       $XF_1(t_{end}) = Finalpos$ 
      %       $XF_2(t_{end}) = 0$ 
25     %       $XF_3(t_{end}) = 0$ 

      % Where all of the times indicated have discrete values, e.g.
      corresponding to
      % the controller update rate.

30

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% It should be noted that after the digital switch times are fixed, the  
constraint

% equations derived from the equations above form a linear set of  
equations in

5       % the unknown relative voltage levels L1, L2 and L3 and any standard  
linear

% method can be used to solve for the relative voltage levels. In the  
equations

10       % for (L1, L2 and L3) that follow, the solution was obtained by algebraic  
% means (and are not particularly compact.)

% compute new relative voltage step levels

% L1, L2 and L3 are nominally assigned to "1", "-2" and "+2",  
respectively

15   s1 = X \* (exp(-et3 \* b) \* exp(-et2 \* a) + exp(-et3 \* a) + exp(-et2 \* b) - exp(-et2  
      \*b) \* exp(-et3 \* a) - exp(-et2 \* a) - exp(-et3 \* b));

s2 = 1 / (et2 \* exp(-et1 \* b) \* exp(-et3 \* a) + exp(-et2 \* b) \* et3 \*  
      exp(-et1 \* a) - et2 \* exp(-et3 \* a) - et2 \* exp(-et1 \* b) - et3 \*  
      exp(-et1 \* a) - exp(-et2 \* b) \* et3 + exp(-et3 \* b) \* et1 \* exp(-et2 \*  
20   a) + exp(-et3 \* a) \* et1 + exp(-et2 \* b) \* et1 - exp(-et2 \* b) \* et1 \*  
      exp(-et3 \* a) - et3 \* exp(-et1 \* b) \* exp(-et2 \* a) - exp(-et2 \* a) \*  
      et1 - exp(-et3 \* b) \* et1 - exp(-et3 \* b) \* et2 \* exp(-et1 \* a) + et3 \*  
      exp(-et1 \* b) + et2 \* exp(-et1 \* a) + exp(-et3 \* b) \* et2 + et3 \*  
      exp(-et2 \* a)) / A;

25

L1 = s1 \* s2;

s1 = 1 / (et2 \* exp(-et1 \* b) \* exp(-et3 \* a) + exp(-et2 \* b) \* et3 \*  
      exp(-et1 \* a) - et2 \* exp(-et3 \* a) - et2 \* exp(-et1 \* b) - et3 \*  
30   exp(-et1 \* a) - exp(-et2 \* b) \* et3 + exp(-et3 \* b) \* et1 \*

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exp(-et2 * a) + exp(-et3 * a) * et1 + exp(-et2 * b) * et1 -
exp(-et2 * b) * et1 * exp(-et3 * a) - et3 * exp(-et1 * b) *
exp(-et2 * a) - exp(-et2 * a) * et1 - exp(-et3 * b) * et1 - exp(-et3 *
b) * et2 * exp(-et1 * a) + et3 * exp(-et1 * b) + et2 * exp(-et1 * a) +
5      exp(-et3 * b) * et2 + et3 * exp(-et2 * a)) * X;
s2 = (exp(-et2 * b) * exp(-et1 * a) - exp(-et1 * a) - exp(-et2 * b) -
      exp(-et1 * b) * exp(-et2 * a) + exp(-et1 * b) + exp(-et2 * a)) / A;
L3 = s1*s2;

10  s1 = exp(-et1 * a) - exp(-et3 * a) + exp(-et3 * b) - exp(-et1 * b) -
      exp(-et3 * b) * exp(-et1 * a) + exp(-et1 * b) * exp(-et3 * a);
s2 = X / (et2 * exp(-et1 * b) * exp(-et3 * a) + exp(-et2 * b) * et3 *
      exp(-et1 * a) - et2 * exp(-et3 * a) - et2 * exp(-et1 * b) - et3 *
      exp(-et1 * a) - exp(-et2 * b) * et3 + exp(-et3 * b) * et1 * exp(-et2 *
15  a) + exp(-et3 * a) * et1 + exp(-et2 * b) * et1 - exp(-et2 * b) * et1 * exp(-
et3 * a) - et3 * exp(-et1 * b) * exp(-et2 * a) - exp(-et2 * a) * et1 - exp(-et3 *
b) * et1 - exp(-et3 * b) * et2 * exp(-et1 * a) + et3 *
      exp(-et1 * b) + et2 * exp(-et1 * a) + exp(-et3 * b) * et2 + et3 *
      exp(-et2 * a)) / A;

20
L2 = s1 * s2;

% convert accumulated voltage steps to sequential voltage level
V1 = Vmax * (L1);
25  V2 = Vmax * (L1 + L2);
V3 = Vmax * (L1 + L2 + L3);

% END OF PSEUDO CODE

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